

(amended) PATENT CLAIMS

1. A fired ceramic moulded body, made of a composition which comprises at least one purely magnesitic component and at least one component containing CaO, all in a grain size < 8 mm which has the following oxidic analysis:
  - a) 50 to 90 % by weight MgO,
  - b) 8 to 40 % by weight CaO,
  - c) 1 to 8 % by weight Fe<sub>2</sub>O<sub>3</sub>,
  - d) up to 10 % by weight others,the sum total of a) to d) being 100 % by weight, providing, after firing, a test value T<sub>0,5</sub> according to DIN EN 993-8 (1997) of between 1,400 and 1,700 °C.
2. Moulded body according to claim 1 with a raw density of > 3 g/cm<sup>3</sup>.
3. Moulded body according to claim 1 with an open porosity of < 14 % by volume.
4. Moulded body according to claim 1 in which the purely magnesitic component has a degree of purity of > 90 % by weight MgO.
5. Process for the production of a fired ceramic, Fe<sub>2</sub>O<sub>3</sub> comprising moulded body, with a test value T<sub>0,5</sub> according to DIN EN 993-8 (1997) of between 1400 °C and 1700 °C, according to which a composition is used, comprising at least one purely magnesitic and at least one component containing CaO, all in a grain size of < 8 mm and which has the following oxidic analysis:
  - a) 50 to 90 % by weight of MgO,
  - b) 8 to 40 % by weight of CaO,
  - c) 1 to 8 % by weight of Fe<sub>2</sub>O<sub>3</sub>,

the total sum of a) to d) being 100 %, and forming dicalciumferrite as a secondary phase after firing at a temperature > 1400°C.

6. Process according to claim 5 in which at least one CaO-containing component of the composition has a grain size of > 2 mm.
7. Process according to claim 5 in which at least one CaO-containing component of the composition has a grain size of < 5 mm.
8. Process according to claim 5 in which the MgO-containing component of the composition with a degree of purity of > 90 % by weight has a grain size of < 5 mm.
9. Process according to claim 5 in which the MgO-containing component of the composition with a degree of purity of > 90 % by weight has a grain size of < 2 mm.
10. Process according to claim 5 in which the MgO-containing component of the composition with a degree of purity of > 90 % by weight has a grain size of < 0.3 mm.
11. Process according to claim 5 in which the mean grain size ( $d_{50}$ ) of the CaO-containing component of the composition is greater than the mean grain size ( $d_{50}$ ) of the MgO-containing component of the composition with a degree of purity > 90 % by weight.

12. Process according to claim 5 in which the grain size ( $d_{95}$ ) of the CaO-containing component of the composition is greater than the grain size ( $d_{95}$ ) of the MgO-containing component of the composition with a degree of purity of > 90 % by weight.
13. Process according to claim 5 in which at least one CaO-containing component of the composition has a grain size of < 1 mm.
14. Process according to claim 5 in which at least one CaO-containing component of the composition has a grain size of < 0.3 mm.
15. Process according to claim 5 with a  $\text{Fe}_2\text{O}_3$  content of the composition of > 1.5 % by weight.
16. Process according to claim 5 with a  $\text{Fe}_2\text{O}_3$  content of the composition of > 2 % by weight.
17. Process according to claim 5 with a proportion of an MgO-CaO fused grain component in the composition.
18. Process according to claim 5 in which the oxidic analysis of the composition exhibits at least one of the following oxides:  $\text{MnO}$ ,  $\text{TiO}_2$ ,  $\text{ZrO}_2$ ,  $\text{SiO}_2$ .
19. Process according to claim 5, in which the purely magnesitic component has a degree of purity of > 90 % by weight.
20. Use of a moulded body according to claim 1 for lining of a rotary kiln.